

APPLICATION  
FOR  
UNITED STATES LETTERS PATENT

TITLE: RAPID MULTISLICE BLACK BLOOD DOUBLE-  
INVERSION RECOVERY TECHNIQUE FOR BLOOD  
VESSEL IMAGING

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with a rapid acquisition with relaxation enhancement (RARE) readout has been successfully applied in vivo for vessel wall imaging of different vascular beds. Fayad et al., Clinical imaging of the high-risk or vulnerable atherosclerotic plaque, *Circulation Research* 2001;89:305-316. Yuan et al., Carotid Atherosclerotic Plaque: Noninvasive MR Characterization and Identification of Vulnerable Lesions, *Radiology* 2001;221:285-99.

Improved DIR sequences to reduce examination time were recently developed. Song et al., Multislice double inversion pulse sequence for efficient black-blood MRI, *Magn Reson Med* 2002;47:616-20. Parker et al., Improved efficiency in double-inversion fast spin-echo imaging, *Magn Reson Med*, 2002;47:1017-1021. Yarnykh et al., Multislice double inversion-recovery black-blood imaging with simultaneous slice reinversion, *J Magn Reson Imaging* 2003;17:478-83.

Song et al. demonstrated a dual-slice DIR technique. The DIR preparation module was modified to include one non-selective and two slice-selective inversion pulses. Following the DIR preparation module, k-space lines from two slices were acquired. A single DIR preparation module was gated to each cardiac cycle (i.e., the repetition interval, TR, was equal to 1 RR interval). Song et al. suggested that data for additional slices could be acquired, but taught that the number of slices possible is limited by the time window during which blood magnetization is nullified. A later publication by Song et al. taught acquiring five slices after each DIR module, using a very short image acquisition sequence, and a DIR repetition interval equal to one RR interval. Song, Highly efficient double-inversion spiral technique for coronary vessel wall imaging, *Proceedings of ISMRM* 2002;1566.

Parker et al. and Yarnykh et al. taught that improved efficiency could be had by reducing the inversion interval (TI) for nulling the blood signal by administering a repetitive series of DIR modules (Fig. 1d) at a repetition interval short enough to put two DIR modules within each RR interval, but both publications taught that only a single slice of image data should be acquired after each DIR module. Parker et al. criticized the multislice technique proposed by Song et al. because "only one of the slices imaged will have the appropriate inversion time to null the signal from blood."

## Summary

We have discovered that significantly faster image acquisition can be achieved with DIR imaging of blood vessels by administering a series of DIR preparation pulse modules at a repetition interval short enough that at least two DIR preparation pulse modules generally occur within each RR interval, and by acquiring image data for a plurality of slices following each DIR module. Acquiring image data for a plurality of slices means that image data is acquired at times other than when blood magnetization is perfectly nulled (at exactly  $TI_0$ ), but our research has established that the resulting images have acceptable image quality.

Preferred implementations of the invention may incorporate one or more of the following. The repetition interval for the administered DIR modules may be less than about 500 msec. The inversion time  $TI_0$  may be less than about 190 msec. Image data acquisition may extend across an interval that begins before and ends after the inversion time  $TI_0$ . Image data acquisition may occur in an interval when longitudinal magnetization of blood is reduced to at least 10 percent of full longitudinal magnetization. Image data acquisition may be cardiac triggered or untriggered. The DIR modules may comprise an inversion pulse followed by a reinversion pulse, and the reinversion pulse may reinvert a plurality of the slices to be imaged. The DIR modules may consist of an inversion pulse followed by reinversion pulse that reinverts all of the slices to be imaged. The repetition time (TR) of blood may be disassociated from the TR of the rest of the tissues in the imaging slice.

Other features and advantages of the invention will be apparent from the following detailed description, and from the drawings and claims.

## Brief Description of the Drawings

FIG. 1 is a pulse sequence diagram for a preferred implementation of the invention.

FIG. 2 is an enlarged diagram of one DIR module and associated image acquisition modules of FIG. 1 (the portion of FIG. 1 enclosed by dashed lines).

FIG. 3 is a plot showing the relationship between the repetition interval TR of the DIR modules and the inversion time  $TI_0$  of blood.

FIG. 4 is a plot showing the relationship between the time after the DIR inversion pulse and the longitudinal magnetization.

### Detailed Description

5        There are a great many possible implementations of the invention, too many to describe herein. Some possible implementations that are presently preferred are described below. It cannot be emphasized too strongly, however, that these are descriptions of implementations of the invention, and not descriptions of the invention, which is not limited to the detailed implementations described in this section but is  
10        described in broader terms in the claims.

      The descriptions below are more than sufficient for one skilled in the art to construct the disclosed implementations. Unless otherwise mentioned, the processes and manufacturing methods referred to are ones known by those working in the art

      In a preferred implementation shown in FIGS. 1 and 2, an ECG-triggered pulse  
15        sequence is used. The sequence includes two DIR preparation pulse modules within each RR interval, and acquisition of data from three slices (e.g., S11, S12, S13) follows each DIR module. Image acquisition is done using a rapid acquisition with relaxation enhancement (RARE) pulse sequence. Each group of acquisition sequences (e.g., S11, S12, S13) following a DIR module is known herein as a rapid extended coverage (REX)  
20        module. The REX module of FIGS. 1 and 2 has three data acquisition sequences for three slices, but other REX modules may acquire data for as few as two slices or for more than three slices.

      The DIR module includes two 180-degree adiabatic hyperbolic secant RF pulses: nonselective and selective. The non-selective RF pulse inverts the magnetization of the  
25        whole body. The selective 180° pulse is designed to cover a volume that consists of 120% of the entire slab of  $N_{SL}$  slices, including inter-slice gaps. The thickness of the slab-selective 180° pulse ( $\Delta_{Sel180^\circ}$ ) was calculated as shown below.

$$\Delta_{Sel180^\circ} = (N_{SL} * \Delta_z + (N_{SL} - 1) * Gap) * 1.2 ,$$

      where  $\Delta_{Sel180^\circ}$  is the thickness of slab-selective 180 degree reinversion pulse,  $N_{SL}$  is the  
30        number of slices,  $\Delta_z$  is the thickness of each slice, and Gap is the slice separation.

The sequence acquisition block (REX module) consists of one DIR module followed by multiple (2 to 5) RARE slice readouts. In one implementation, 4-9 REX modules were acquired in 2-RR intervals (the RR interval is the time interval between two consecutive heart beats), yielding 16-20 closely spaced slices. FIG.1 shows the pulse sequence for 18 slices with 6 REX 3-slice modules.  $TI_0$  spans the time from the non-selective RF pulse (inverting the magnetization of the blood) to the middle of the slice readouts in order for them to be as close to the null point of blood as possible.

TR for any slice ( $TR_{SI}$ ) equals 2-RR intervals (typically 1600 ms), and is different from the TR of dark blood ( $TR_{DB}$ ), determined by the time between two successive DIR modules.

$$TR_{DB} = \frac{2RR}{N_{REX}},$$

where  $N_{REX}$  is the number of REX modules.

Reduction in  $TR_{DB}$  leads to a decrease in dark blood  $TI_0$  according to the formula:

$$TI_0 = T_1 * (\ln(2) - \ln(1 + e^{-TR_{DB}/T_1})),$$

where  $T_1$  is the relaxation time of blood ( $T_1 = 1200\text{ms}$  at 1.5T).

The relationship between  $TR_{DB}$  and  $TI_0$  of blood, when its signal is nulled is illustrated in FIG. 3. One dummy scan can be performed prior to data acquisition to allow for steady-state inversion recovery.

The fill time between two consecutive REX modules is  $\tau$ , as shown by the equation below.  $\tau$  (10-50ms) is added to achieve equal time spacing between REX modules, thereby keeping  $TR_{DB}$  constant.

$$\tau = TR_{DB} - (TI_0 + T_{DIR} + (0.5 + TF) * (N_{SL} * esp)),$$

where  $TR_{DB}$  is the TR of dark blood,  $TI_0$  is inversion time,  $T_{DIR}$  is the duration of the DIR module ( $\approx 28\text{ ms}$ ),  $N_{SL}$  is number of slices,  $esp$  is the echo spacing,  $TF$  is the turbo factor.

One experiment using the described implementation proceeded as follows:

Studies were performed on a 1.5T Siemens Sonata whole body MR system (Siemens AG, Erlangen, Germany) with maximum gradient amplitude of 40 mT/m and slew rate of 200

mT/m/ms running Numaris 4.0. The integrated body coil was used for RF transmission, while a circularly polarized six-channel body array was used for signal reception. Aortic vessel wall MR was performed in 5 healthy adults subjects (aged 27-39 years) without known history of coronary artery disease as approved by the institutional review board.

- 5 The subjects were positioned headfirst; supine in the magnet bore. Three surface ECG electrodes were placed on the subjects' chest for data acquisition triggering.

Initial scout images in three orthogonal planes were used to locate the descending aorta in the subjects. During aortic wall imaging, the subjects were asked to hold their breath on inspiration when possible. Multislice protocols with 16, 18, and 20 slices were developed. Other imaging parameters were: echo-spacing (*esp*) of 4.9ms; echo-time (TE) of 4.9 ms, acquisition matrix size of 256 x 256, slice thickness of 3 mm, slice separation of 0.3 mm, data acquisition bandwidth of 488 Hz/pixel, one signal average, and a field of view (FOV) of 250 mm were used. The slice excitation order was descending (from head to foot, along the flow direction) for aortic protocols. The slice readout time ( $\approx esp*TF$ ) ranged between 44 and 64 ms. This ensured minimum vessel wall motion and blurring along the phase encoding direction. Turbo factors (9 to 13) were maximized for a given number of slices to fit the readouts within the TR interval.

A variety of REX DIR-RARE implementations of the invention were quantitatively compared to the images of conventional single slice RARE sequence with 16, 18, and 20 slices. The following table summarizes the implementations examined.

Sequence type	Number of slices / REX modules	Turbo factor	TR of blood (2RR/N <sub>REX</sub> , ms)	TI <sub>0</sub> (ms)	Total readout time (ms)	Acquisition time (RR-intervals)
REX multislice DIR-RARE	16 slices 4 REX modules	13	400	183	265	42
	16 slices 8 REX modules	13	200	96	132	42

	18 slices 6 REX modules	11	267	126	170	50
	18 slices 9 REX modules	11	177	85	113	50
	20 slices 4 REX modules	9	400	183	234	60
	20 slices 5 REX modules	9	320	149	187	60
Single slice conventio nal DIR- RARE (Prior art)	16 slices	13	1600	551	67	642
	18 slices	11	1600	551	57	866
	20 slices	9	1600	551	47	1162

In the implementations described in the table, the slice repetition interval, TR, is 2RR intervals. The T1 of blood was assumed to be 1200 msec at 1.5T, and a 2 RR interval was assumed to be 1600 msec. An acquisition matrix of 256x256 was used.

- 5           The single slice DIR-RARE sequence consisted of a DIR module followed by acquisition of a single slice in one triggering period (2-RR). The number of slices, as well as other MR imaging parameters of the single slice sequence (2-RR triggering interval, TE, matrix size, slice thickness and separation, bandwidth, FOV, TF) were chosen to be the same as those of the REX multislice sequence in order to equitably
- 10       compare the quality of the images of both methods.

With DIR imaging techniques, the blood flowing into the imaging plane after the  $TI_0$  interval has zero longitudinal magnetization due to the prior application of the non-selective inversion pulse. In the experiment, the slices were acquired along the blood



flow direction (from head to foot) to augment outflow effects and hence improve blood suppression. The second slab selective RF pulse in the DIR module reinverted the magnetization of the whole slab of interest (16 to 20 slices), not just the slices imaged after the respective DIR module. This avoided the incomplete recovery of the longitudinal magnetization from the rest of the slices in the imaging slab during the time between two successive DIR modules (e.g., 177 to 400 msec) and resulting loss of muscle signal (SNR).

Typical proton density weighted images from 18 slices in 6 REX 3-slice modules showed flowing blood to appear consistently dark in the descending aorta as shown by the arrows. The image quality and acquisition times for the implementation of the invention (the rapid multislice DIR-RARE sequence) were compared with those for the conventional single slice DIR-RARE. The implementation of the invention demonstrated improved image quality as compared to the single slice sequence. Contrast to noise ratios (CNR) of the implementation were not significantly different from those of single slice DIR-RARE. The speed of the implementation allowed breath hold acquisition for up to 18 slices in healthy volunteers. All 5 healthy subjects held their breath for sequence protocols lasting 45 seconds or less, but breath hold of 45 seconds might not be feasible clinically. However, for the REX sequence the breath hold is optional and is not necessary for successful use. Time improvement factors (ratio between acquisition time of the single slice and corresponding multislice sequences of the implementation of the invention) ranged from 12.25 (16 slice protocol) to 16.54.

The described implementation of the invention separates the TR of the imaging slice from the TR of the blood by introducing multiple DIR modules within 2-RR intervals (TR of slice). The time interval between two successive DIR modules is the TR of blood.

In the described implementation, the time window during which the signal from blood is sufficiently suppressed (within 10% of the perfect null point) was approximately 250 msec. FIG. 4 shows the relationship between time after application of the DIR inversion pulse and the longitudinal magnetization of the inverted blood (for a  $TR_{DB}$  of 267 msec. The dark blood time window in the figure is the time interval over which blood magnetization is suppressed to 10 percent or less. For the multi-slice

implementations described herein, the total readout times ranged from 113 to 265 msec, enabling their acquisition to fit into this time window.

Many other implementations of the invention other than those described above are within the invention, which is defined by the following claims. The following are just a few examples of the many other implementations possible:

Many other image acquisition pulse sequences other than RARE can be used.

We have used the terminology REX module to refer to a DIR module and associated image acquisition sequences. But this is just a choice of terminology, and does not limit the type of DIR module or image acquisition sequence used. Many different DIR modules and many different acquisition sequences could be used within a REX module, and image data for many different numbers of slices can be acquired by one REX module.

Field of view reduction techniques, such as selective presaturation pulses, could be employed with some implementations of the invention, as these techniques could improve the resolution of black blood imaging to a level that would allow vessel wall segmentation.

Three-dimensional (3D) image acquisition could be employed with some implementations. Advantages of 3D acquisition include better excitation slice profile and better SNR. However, any motion, which is not compensated by gating, has the potential to corrupt all slices in the scan, and a wrapping artifact may be present in the Fourier encoded 3D imaging.

Multi-contrast imaging (T1, T2, and PD weighting) is possible with some implementations. For T1-weighted images it may be possible to image up to 10 slices per TR interval. In combination with field of view reduction techniques, more efficient k-space coverage (e.g., spiral readouts, and parallel imaging, it may be possible to image the entire length of the coronary arteries in a single breath hold acquisition.

Other forms of inversion pulses can be used other than the adiabatic secant pulses described. Adiabatic pulses are not necessary. The initial inversion pulse could be the usual hard pulse taught in the literature for DIR imaging.

What is claimed is: